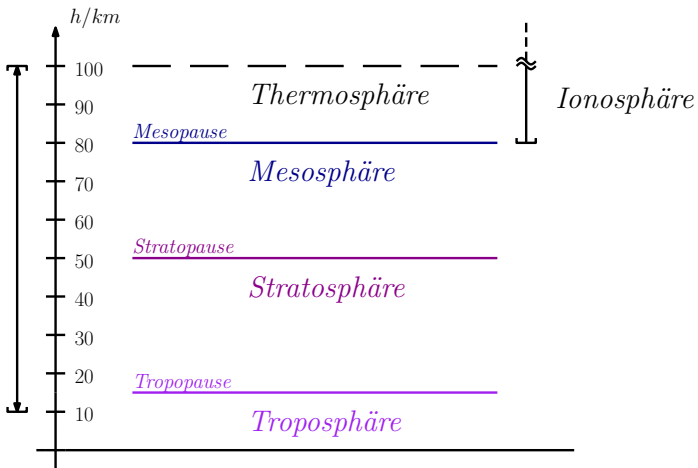


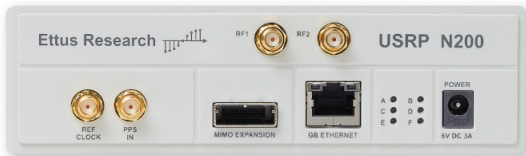
Low Cost Radar-Acquisition with USRP-N200 in Atmospheric Research

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- $f_{S, \text{FPGA}} = 100 \text{MHz}$ Sample-Rate
- $f_{S, \text{DAC}} = 400 \text{MHz}$ Sample-Rate
- $f_{\text{TX}} \in \{0, 250\} \text{MHz}$ (FPGA+DAC CORDIC)
- $f_{\text{RX}} \leq 50 \text{MHz}$ (32.55MHz) no Aliasing
- $f_{\text{RX}} \geq 50 \text{MHz}$ (53.50MHz) Aliasing

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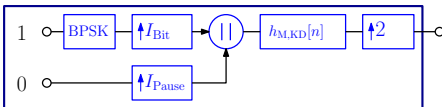
Receiving with USRP-N200

② Results and Future

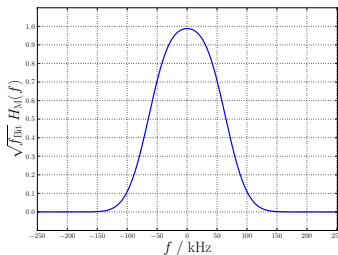
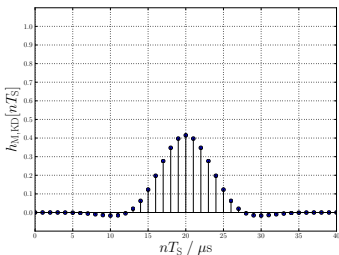
Results

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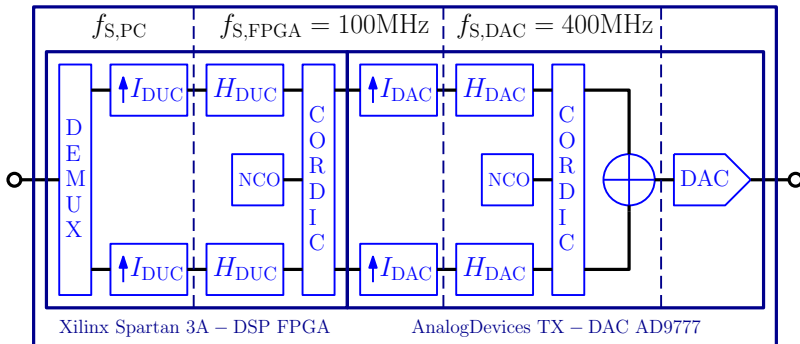
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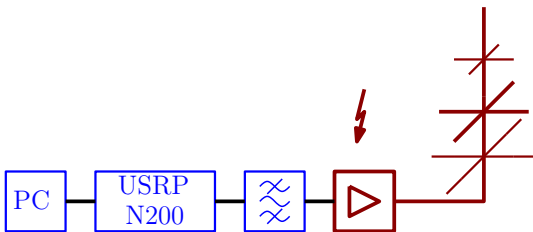
PC TX – Signal Synthesis



Transmitting with USRP-N200



USRP – N200 TX – Chain

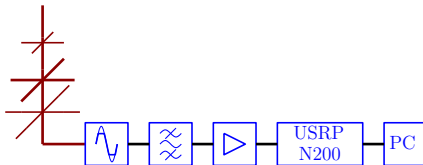


- Bandpass filters out DAC Spuries & Intermodulations
- Linear (Tube/Solid-State)-Amplifier up to 10kW

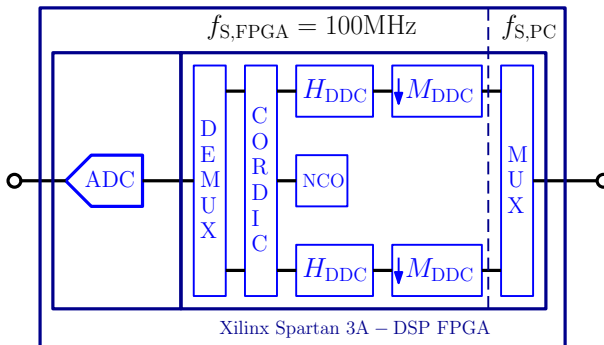
Signal Scatterer

- Clouds
- Airplanes
- Ground- / Sea-Clutter
- Inhomogenous Refractive-Index $n(\mathbf{r}, t)$
- Inhomogenous Electron-Densities $\rho(\mathbf{r}, t)$
- Plasma-Trail from Meteors

Receiving with USRP-N200



- Limiter cares about too much Input-Power
- Bandpass for unwanted Frequency components
- Pre-Amplifiers puts Signal-Amplitude up to Dynamic-Range of ADC



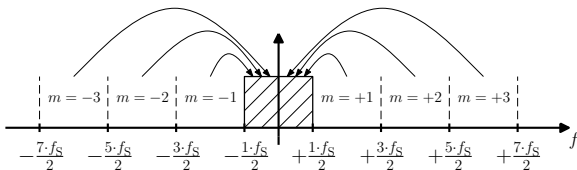
USRP - N200 RX - Chain

- the received analog signal with $f_{RX}(\mathbf{r}, t) = f_{CF} + f_D(\mathbf{r}, t)$ is:

$$\begin{aligned} u_E(t) &= \hat{u}_E(t) \Re\{e^{2\pi j \cdot f_{RX}(\mathbf{r}, t) \cdot t} e^{j \cdot \varphi_{RX}(t)}\} + w_E(t) \\ &= \hat{u}_E(t) \Re\{e^{2\pi j \cdot f_{CF} \cdot t} e^{2\pi j \cdot f_D(\mathbf{r}, t) \cdot t} e^{j \cdot \varphi_{RX}(t)}\} + w_E(t) \end{aligned}$$

- when the signal is sampled by the ADC with $f_{S, FPGA} = f_S$ the following situation can happen:

$$f_{CF} = \text{const} = \begin{cases} f_{DDC} & , \text{no aliasing} \\ f_{DDC} + m f_S & , \text{aliasing for } m \in \mathbb{Z} \setminus \{0\} \end{cases}$$



- and the Center-Frequency for Down-Conversion is:

$$\frac{(2m - 1)f_s}{2} < f_{CF} < \frac{(2m + 1)f_s}{2}$$

$$f_{DDC} = f_{CF} - \underbrace{\left[\frac{2f_{CF} - f_s}{2f_s} \right]}_{=m} f_s$$

- the sampled signal is:

$$u_E[n] = \hat{u}_E[n] \Re\{e^{2\pi j \cdot f_{DDC} T_S \cdot n} e^{2\pi j \cdot f_D[\mathbf{r}, n T_S] T_S \cdot n} e^{j \cdot \varphi_{RX}[n]}\} + w_E[n]$$

- after passing the Cordic, the signal is:

$$\underline{u}_{BP}[n] = u_E[n] \hat{u}_{DDC} e^{2\pi j \cdot f_{DDC} T_S \cdot n} e^{j \cdot \varphi_{DDC}} + \underline{w}_{BP}[n]$$

- which includes the *baseband* and $2f_{DDC}$ component
- $2f_{DDC}$ vanishes by passing the Decimation-Filter

- the Baseband-Signal can be described by:

$$\begin{aligned} \underline{u}_{\text{BB}}[n] &= \hat{\underline{u}}_{\text{BB}}[n] e^{2\pi j \cdot f_{\text{D}}[\mathbf{r}, n] T_{\text{S}} \cdot n} + \underline{w}_{\text{BB}}[n] \quad \circ \text{---} \bullet \quad \underline{U}_{\text{BB}}(f - f_{\text{D}}[\mathbf{r}, n]) \\ &= I_{\text{BB}}[n] + j \cdot Q_{\text{BB}}[n] \end{aligned}$$

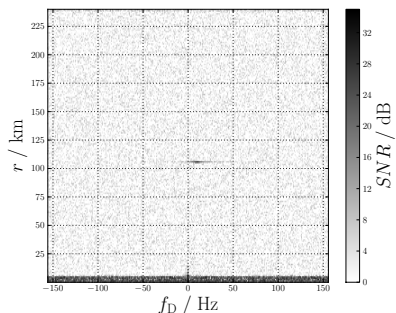
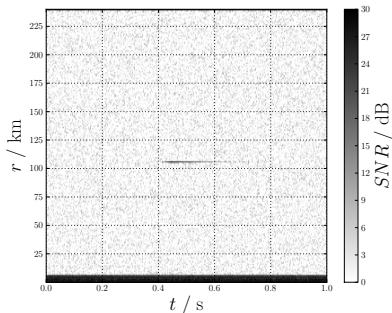
- with the Soft-Condition:

$$|f_{\text{D}}[\mathbf{r}, n]| < \frac{f_{\text{S,PC}}}{2}$$

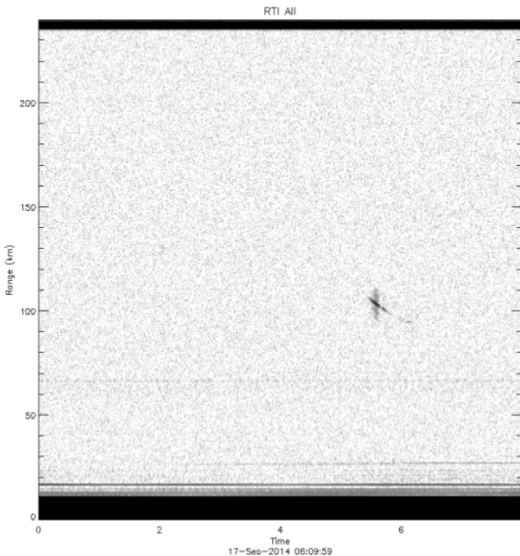
- and with the Hard-Condition:

$$|f_{\text{D}}[\mathbf{r}, n]| < f_{\text{cutoff,matched}}$$

Results



Results



Future

- Interferometry (Range \rightarrow Altitude $\rightarrow \mathbf{v}(\mathbf{r}, t)$)
- Fluctuation Estimation (realtime Coherent- and Incoherent-Integration)
- Deconvolution of overlapped echos
- Spread Spectrum (M-Sequence PRBS - CW)
- Digital Beamforming
- High resolution MST-radar

THANK YOU

